

A short course on

Structural Members

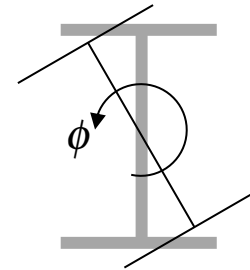
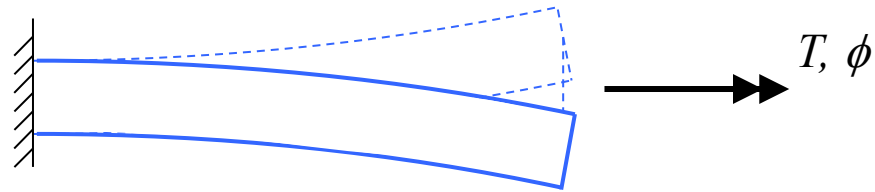
This video:

St. Venant Torsion

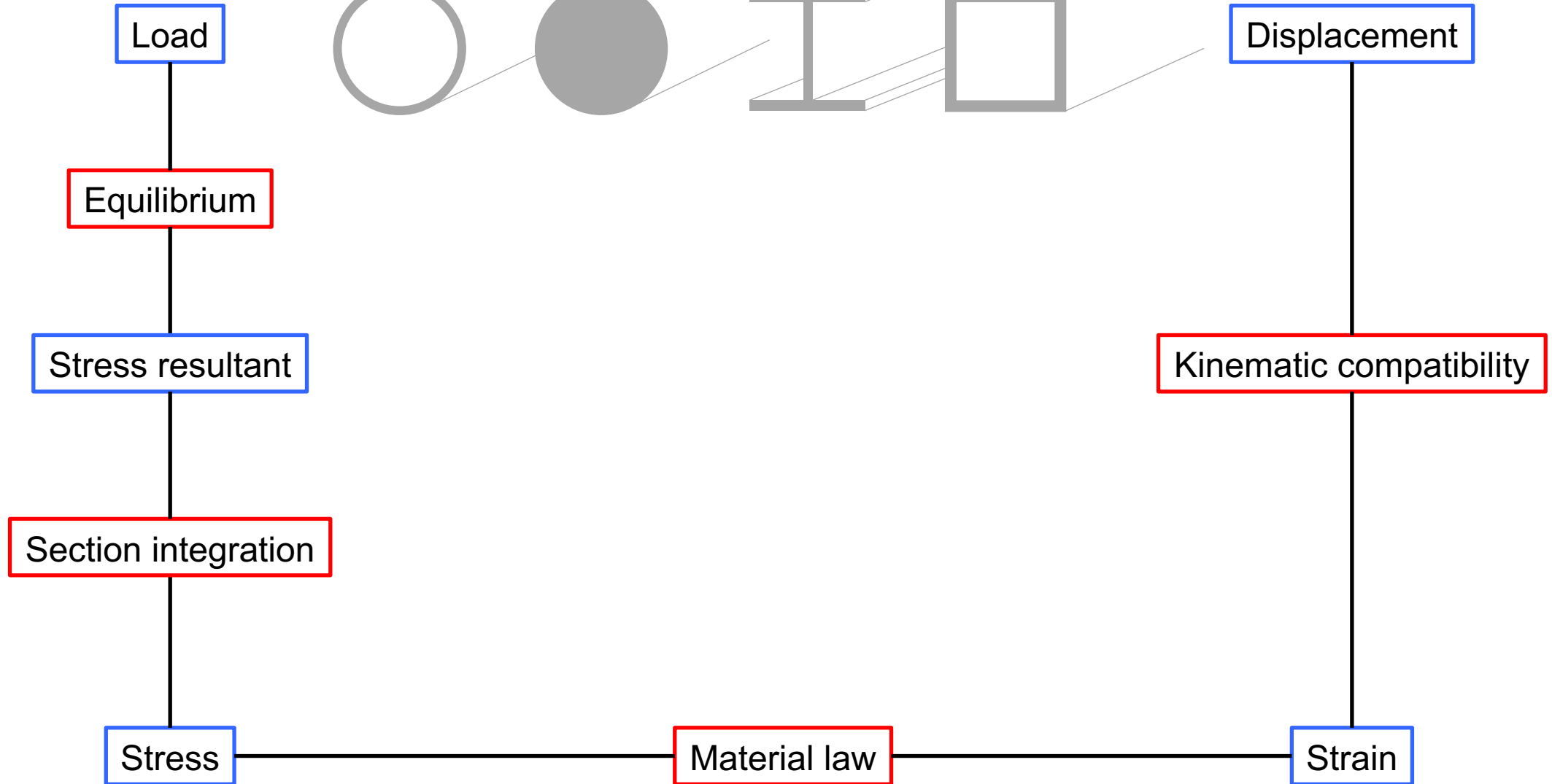
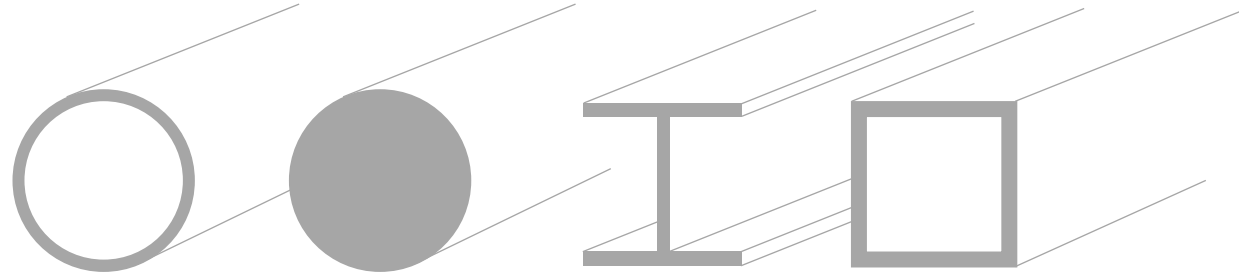
Terje's Toolbox is freely available at terje.civil.ubc.ca

It is created and maintained by Professor Terje Haukaas, Ph.D., P.Eng.,
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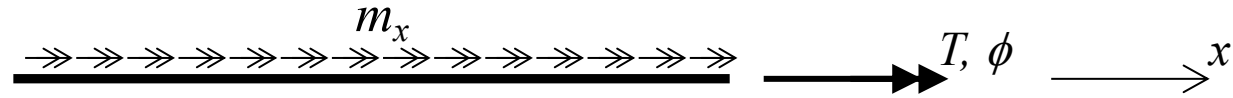
Two Types of Torsion



Ingredients



Notation



x = longitudinal axis

m_x = distributed torque along the member

T = torque, resultant of shear stress

ϕ = rotation about the x -axis

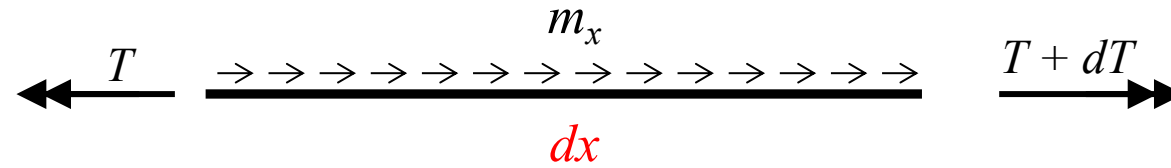
J = cross-section constant for St. Venant torsion

G = shear modulus = $E/(2(1+\nu))$

τ = shear stress

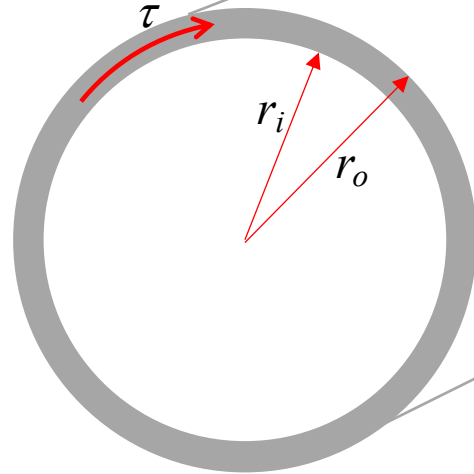
γ = shear strain

Equilibrium



$$m_x \cdot dx - T + T + dT = 0 \quad \Rightarrow \quad m_x = -\frac{dT}{dx}$$

Section Integration



$$T = \int_{r_i}^{r_o} (2\pi r) \cdot \tau \cdot r \cdot dr$$

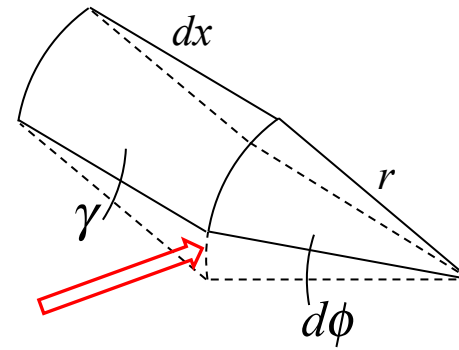
Material Law

$$\tau = G \cdot \gamma$$

$$G = \frac{E}{2(1 + \nu)}$$

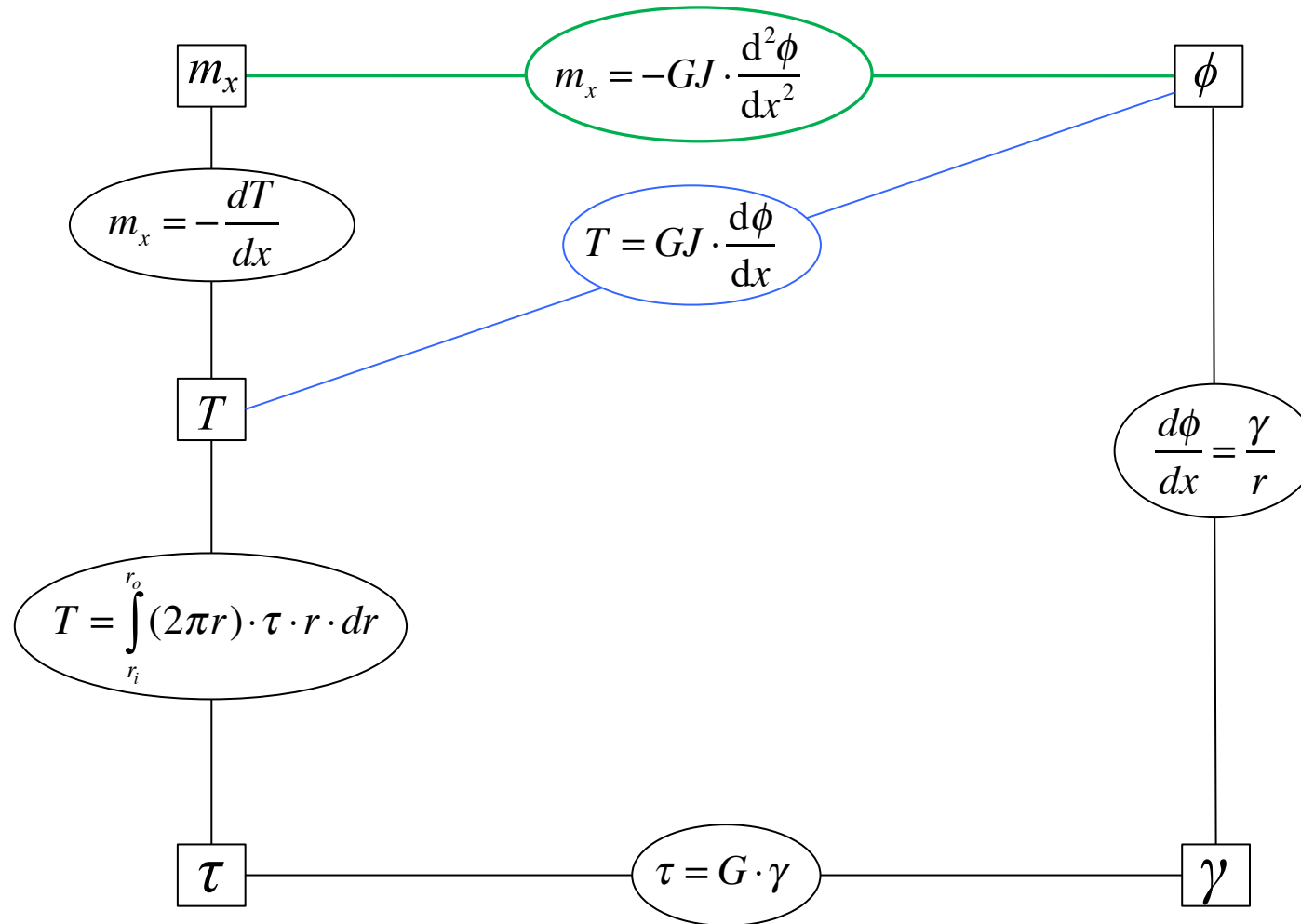
Kinematic Compatibility

$$\frac{d\phi}{dx} = \frac{\gamma}{r}$$



Summary

$$J = \int_{r_i}^{r_o} 2\pi r^3 dr = \frac{\pi}{2} \cdot (r_o^4 - r_i^4)$$



Prandtl's Stress Function

$P(y, z)$

$$\tau_{xy} = \frac{\partial P}{\partial z} = P_{,z}$$

$$\tau_{xz} = -\frac{\partial P}{\partial y} = -P_{,y}$$

$$\sigma_{xx,x} + \tau_{yx,y} + \tau_{zx,z} = 0$$

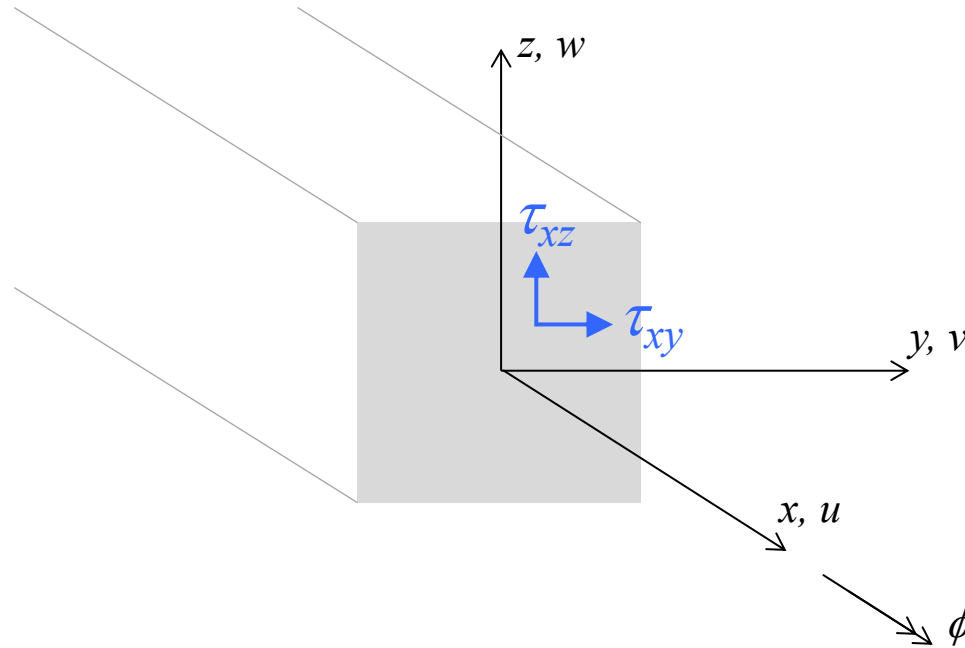
$$\tau_{xy,x} + \sigma_{yy,y} + \tau_{zy,z} = 0$$

$$\tau_{xz,x} + \tau_{yz,y} + \sigma_{zz,z} = 0$$

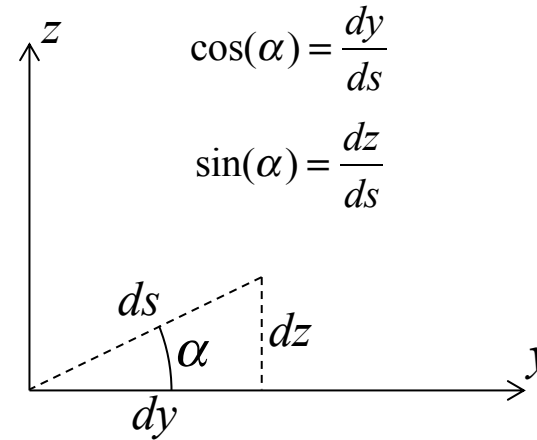
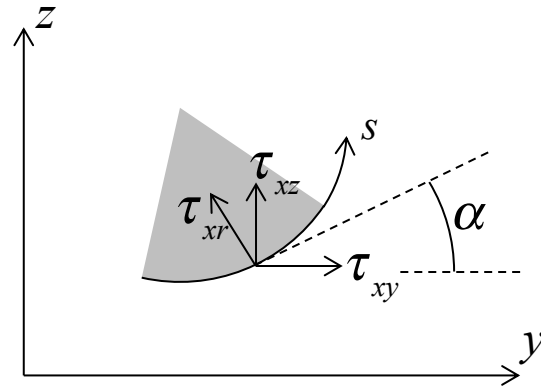
$$\sigma_{xx,x} + \tau_{yx,y} + \tau_{zx,z} = 0 + P_{,zy} - P_{,yz} = 0$$

$$\tau_{xy,x} + \sigma_{yy,y} + \tau_{zy,z} = P_{,zx} + 0 + 0 = 0$$

$$\tau_{xz,x} + \tau_{yz,y} + \sigma_{zz,z} = -P_{,zx} + 0 + 0 = 0$$



Boundary Conditions for Stress Function



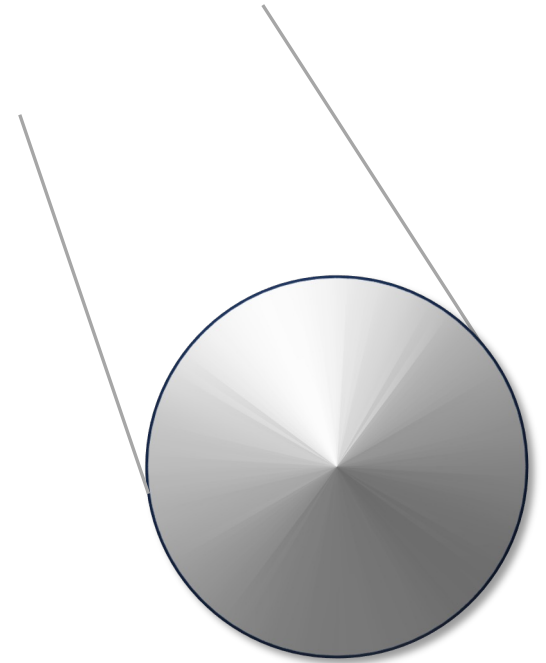
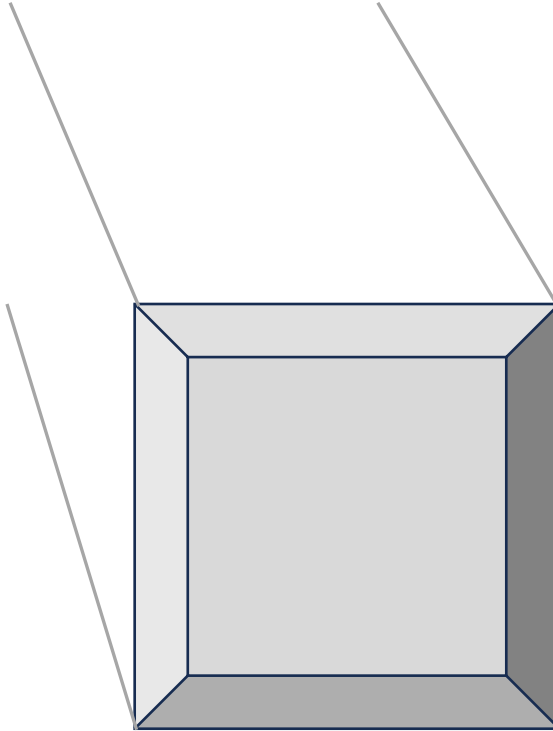
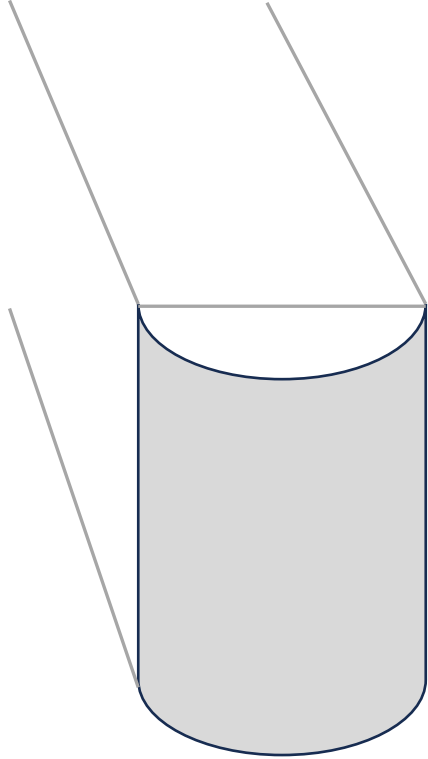
$$\tau_{xr} = 0$$

$$\tau_{xr} = \frac{\partial P(r,s)}{\partial s}$$

$$\frac{\partial P(r,s)}{\partial s} = 0$$

$$\tau_{xr} = \tau_{xz} \cdot \cos(\alpha) - \tau_{xy} \cdot \sin(\alpha) = -\left(\frac{\partial P}{\partial y} \frac{\partial y}{\partial s} + \frac{\partial P}{\partial z} \frac{\partial z}{\partial s}\right) = \frac{\partial P}{\partial s} = 0$$

Membranes



Section Integration

$$T = \int_A (\tau_{xz} \cdot y - \tau_{xy} \cdot z) dA$$

$$T = - \int_A \left(\frac{\partial P}{\partial y} \cdot y + \frac{\partial P}{\partial z} \cdot z \right) dA$$

$$\begin{aligned} T &= - \left(\int_A \frac{\partial P}{\partial y} \cdot y \cdot dA \right) - \left(\int_A \frac{\partial P}{\partial z} \cdot z \cdot dA \right) \\ &= - \left(\oint P \cdot y \cdot d\Gamma - \int_A P \cdot dA \right) - \left(\oint P \cdot z \cdot d\Gamma - \int_A P \cdot dA \right) \\ &= - \underbrace{\oint P \cdot y \cdot d\Gamma}_0 - \underbrace{\oint P \cdot z \cdot d\Gamma}_0 + \int_A P \cdot dA + \int_A P \cdot dA \\ &= 2 \cdot \int_A P \cdot dA \end{aligned}$$

Kinematic Compatibility

$$v = -\phi \cdot z$$

$$w = \phi \cdot y$$

$$\varepsilon_x = \frac{du}{dx} = 0$$

$$\varepsilon_y = \frac{dv}{dy} = 0$$

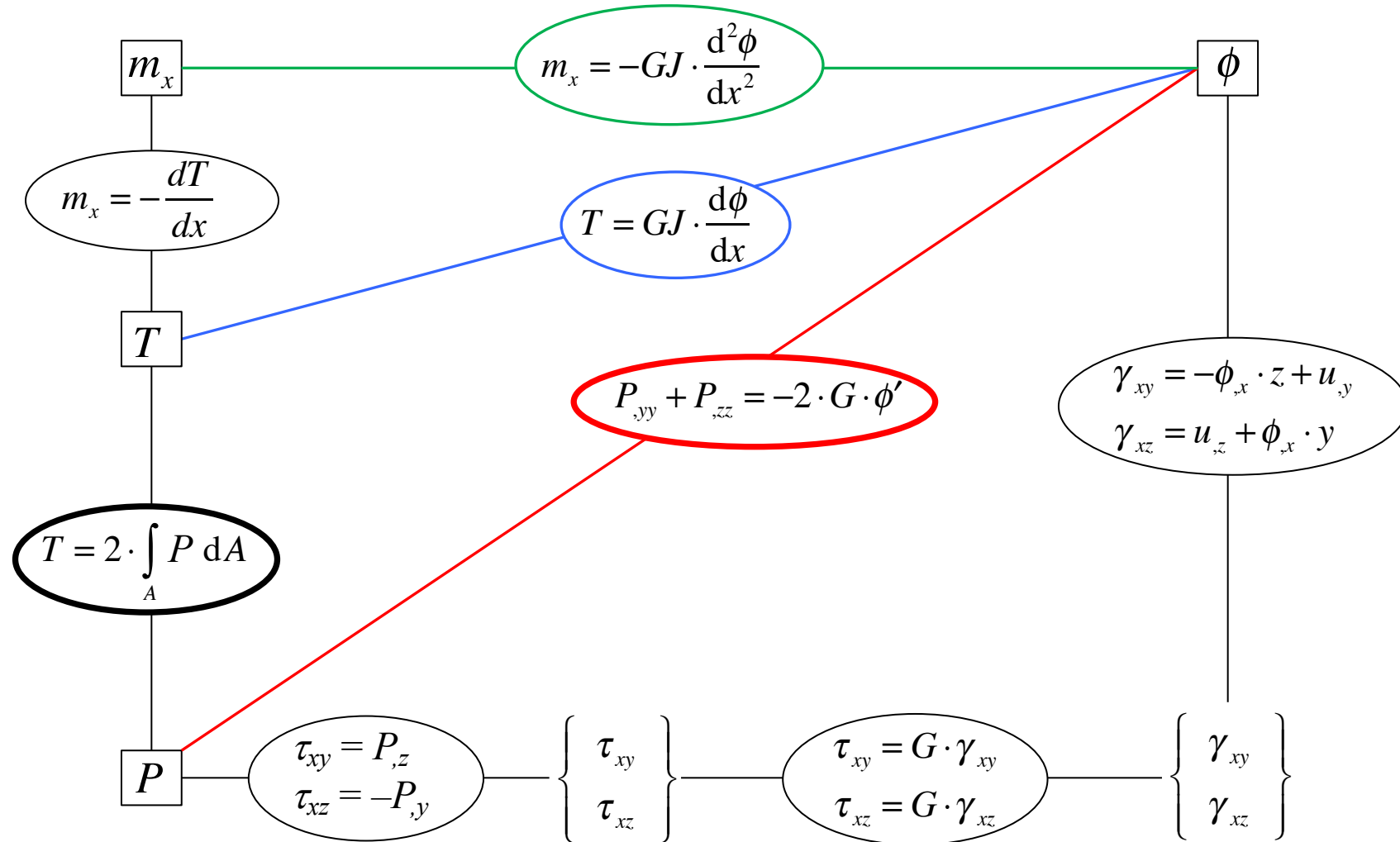
$$\varepsilon_z = \frac{dw}{dz} = 0$$

$$\gamma_{xy} = \frac{dv}{dx} + \frac{du}{dy} = -\frac{d\phi}{dx} \cdot z + \frac{du}{dy}$$

$$\gamma_{xz} = \frac{du}{dz} + \frac{dw}{dx} = \frac{du}{dz} + \frac{d\phi}{dx} \cdot y$$

$$\gamma_{yz} = \frac{dw}{dy} + \frac{dv}{dz} = 0$$

Summary



$$P_{,z} = \tau_{xy} = G \cdot \gamma_{xy} = G \cdot (-\phi_{,x} \cdot z + u_{,y})$$

$$P_{,y} = -\tau_{xz} = -G \cdot \gamma_{xz} = -G \cdot (u_{,z} + \phi_{,x} \cdot y)$$



$$\frac{\partial^2 P(y,z)}{\partial y^2} + \frac{\partial^2 P(y,z)}{\partial z^2} \equiv P_{,yy} + P_{,zz} \equiv \nabla^2 P(y,z) = -2 \cdot G \cdot \phi'$$

Cross-section Analysis

Cross-section constant, J

Shear stress τ_{xy} and τ_{xz}

$$T = GJ \cdot \frac{d\phi}{dx}$$

$$\underbrace{\left(2 \cdot \int_A P \cdot dA \right)}_T = GJ \cdot \underbrace{\left(-\frac{P_{,yy} + P_{,zz}}{2 \cdot G} \right)}_{\phi_{,x}}$$

$$T = 2 \cdot \int_A P \, dA$$

$$P_{,yy} + P_{,zz} = -2 \cdot G \cdot \phi'$$

$$J = -\frac{4 \cdot V}{\nabla^2 P}$$

More lectures:

Terje's Toolbox:

terje.civil.ubc.ca