

A short course on

Cross-section Analysis

This video:

Stress Functions for the Calculation of Cross-section Constant and Stress in Saint Venant Torsion

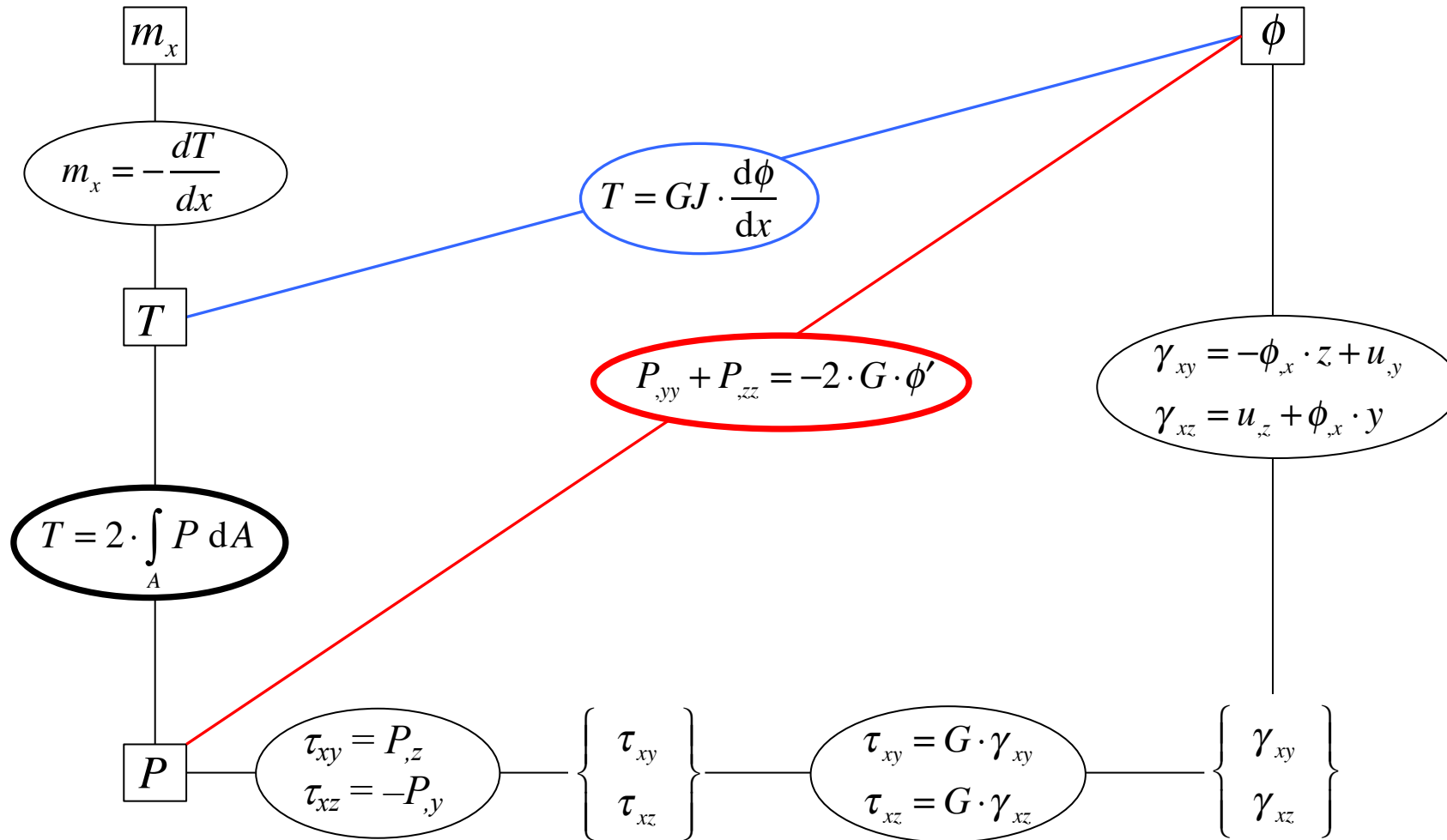
Terje's Toolbox is freely available at terje.civil.ubc.ca

It is created and maintained by Professor Terje Haukaas, Ph.D., P.Eng.,
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Scope

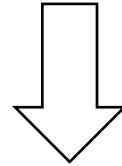
- y_o, z_o = centroid coordinates
- y_{sc}, z_{sc} = shear centre coordinates
- A = cross-section area
- I_y, I_z = moments of inertia
- I_{yz} = product of inertia
- θ = orientation of principal axes
- J = Saint Venant torsion constant
- Ω = omega diagram
- C_w = warping torsion constant
- A_{vy}, A_{vz} = shear area
- σ = axial stress
- τ = shear stress
- q_s = shear flow

Summary

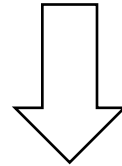


Cross-section constant, J

$$T = GJ \cdot \frac{d\phi}{dx}$$
$$T = 2 \cdot \int_A P \, dA$$
$$P_{,yy} + P_{,zz} = -2 \cdot G \cdot \phi'$$



$$\underbrace{\left(2 \cdot \int_A P \cdot dA \right)}_T = GJ \cdot \underbrace{\left(-\frac{P_{,yy} + P_{,zz}}{2 \cdot G} \right)}_{\phi'}$$



$$J = -\frac{4 \cdot V}{\nabla^2 P}$$

Alternative J

$$\int_{A_\Gamma} P_{,yy} + P_{,zz} dA = -2 \cdot G \cdot \phi_{,x} \int_{A_\Gamma} dA$$

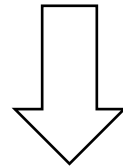
$$\int_{A_\Gamma} P_{,yy} + P_{,zz} dA = \oint_{\Gamma} (P_{,y} dz - P_{,z} dy)$$

$$\oint_{\Gamma} (P_{,y} dz - P_{,z} dy) = \oint_{\Gamma} (\tau_{xz} dz + \tau_{xy} dy) = \oint_{\Gamma} \left(\tau_{xz} \frac{dz}{ds} + \tau_{xy} \frac{dy}{ds} \right) ds = \oint_{\Gamma} \tau_{xs} ds$$

$$T = 2 \cdot \int_A P dA$$

$$T = GJ \cdot \frac{d\phi}{dx}$$

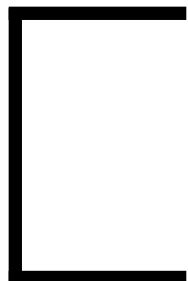
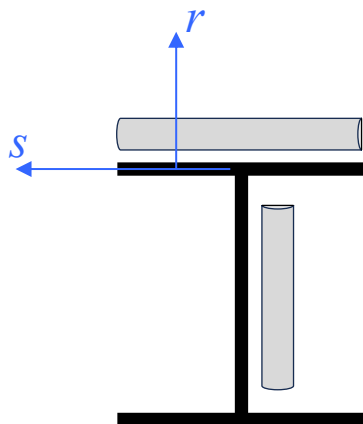
$$\oint_{\Gamma} \tau_{xs} ds = -2 \cdot G \cdot \phi' \cdot A_\Gamma$$



$$J = -\frac{4 \cdot V \cdot A_\Gamma}{\oint_{\Gamma} \tau_{xs} ds}$$

See Bredt's formula later...

Thin-walled, Open



$$P(r, s) = k \cdot \left(1 - 4 \cdot \frac{r^2}{t^2} \right)$$

$$J = -\frac{4 \cdot V}{\nabla^2 P}$$

$$V \equiv \int_A P \cdot dA = \int_{-t/2}^{t/2} \int_{-b/2}^{b/2} k \left(1 - 4 \cdot \frac{r^2}{t^2} \right) ds dr = \frac{2}{3} \cdot k \cdot t \cdot b$$

$$\nabla^2 P \equiv P_{,ss} + P_{,rr} = -\frac{8k}{t^2}$$

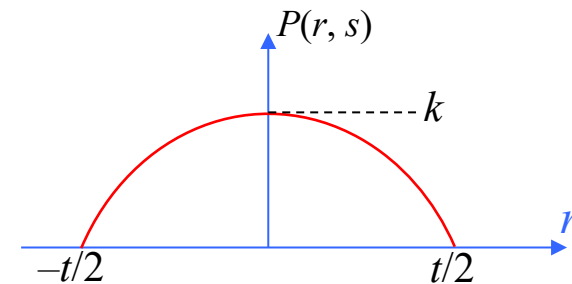
$$\Rightarrow J = \frac{1}{3} \cdot t^3 \cdot b$$

$$\tau_{xs} = P_{,r} = \frac{8k}{t^2} \cdot r$$

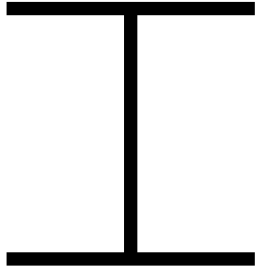
$$\tau_{xr} = -P_{,s} = 0$$

$$T = 2 \cdot \int_A P \cdot dA = 2 \cdot V$$

$$\tau_{xs} = \left(\frac{8 \cdot r}{t_i^2} \right) \cdot k = \left(\frac{8 \cdot r}{t_i^2} \right) \cdot \left(\frac{3 \cdot T}{4 \cdot t \cdot b} \right)$$



Cross-sections with Several Parts



$$T = \sum T_i$$

$$T = \sum \left(GJ_i \cdot \frac{d\phi}{dx} \right) = \frac{d\phi}{dx} \cdot \sum (GJ_i) \equiv \frac{d\phi}{dx} \cdot GJ$$



$$T_i = GJ_i \cdot \frac{d\phi_i}{dx} = \frac{GJ_i}{\sum (GJ_i)} \cdot T$$

$$T_i = 2 \cdot \int_A P \cdot dA = 2 \cdot V_i$$

$$V_i = \frac{2}{3} \cdot k_i \cdot t_i \cdot b_i$$

$$\tau_{xs} = \left(\frac{8 \cdot r}{t_i^2} \right) \cdot k = \left(\frac{8 \cdot r}{t_i^2} \right) \cdot \left(\frac{3 \cdot T_i}{4 \cdot t_i \cdot b_i} \right)$$


 J_i

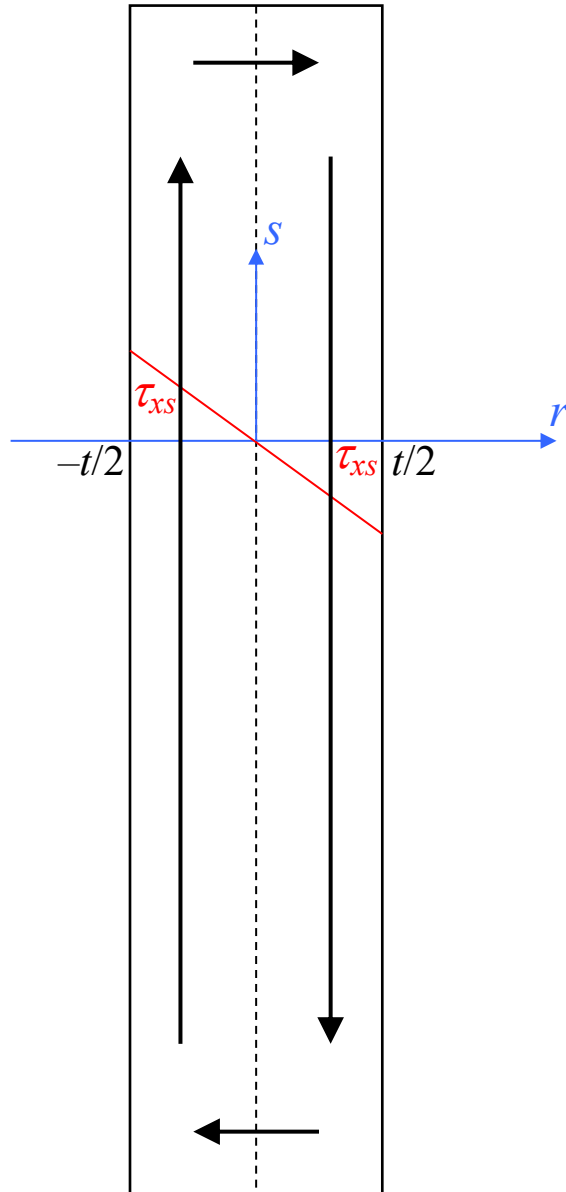
$$GJ = \sum GJ_i$$

$$T_i = \frac{GJ_i}{\sum (GJ_i)} \cdot T$$

$$V_i = T_i / 2 \rightarrow k_i$$

$$\tau_{xs} = \left(\frac{8 \cdot r}{t_i^2} \right) \cdot k_i$$

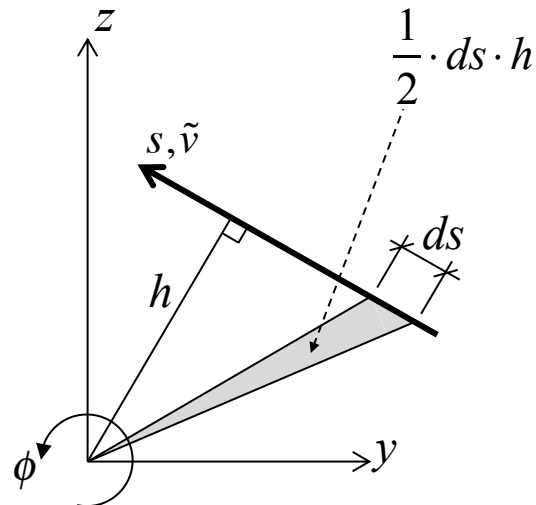
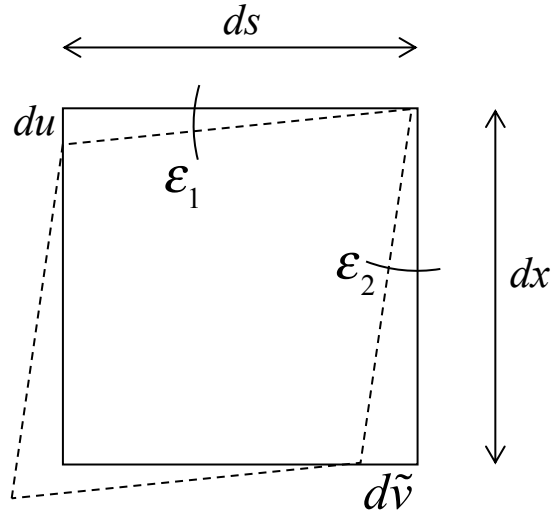
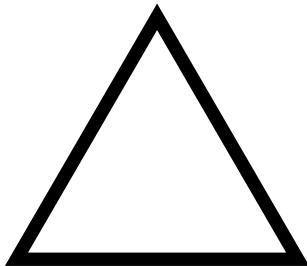
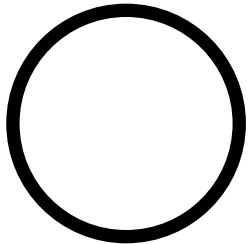
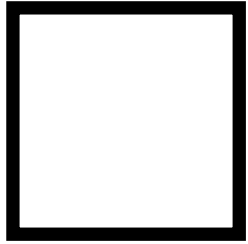
Checking the Torque



$$\tau_{xs} = \frac{8 \cdot \frac{t}{2}}{t^2} \cdot \frac{3 \cdot T}{4 \cdot t \cdot b} = \frac{3 \cdot T}{t^2 \cdot b}$$

$$T = \left(\frac{1}{2} \cdot \tau_{xs} \cdot \frac{t}{2} \right) \cdot b \cdot \frac{2}{3} \cdot t = \frac{T}{2}$$

Closed Cross-sections



$$\oint_{\text{Closed curve}} du = 0$$

$$\gamma_{xs} = \epsilon_{xs,1} + \epsilon_{xs,2} = \frac{du}{ds} + \frac{d\tilde{v}}{dx}$$

$$du = \left(\frac{\tau_{xs}}{G} - \frac{d\tilde{v}}{dx} \right) \cdot ds$$

$$\oint_{\text{Closed curve}} \left(\frac{\tau_{xs}}{G} - \frac{d\tilde{v}}{dx} \right) ds = 0$$

$$\oint_{\text{Closed curve}} \left(\frac{\tau_{xs}}{G} - \frac{d\phi}{dx} \cdot h \right) ds = \oint_{\text{Closed curve}} \frac{\tau_{xs}}{G} ds - \frac{d\phi}{dx} \cdot \oint_{\text{Closed curve}} h ds = 0$$

$$\oint_{\text{Closed curve}} h \cdot ds \equiv 2 \cdot A$$

$$\oint_{\text{Closed curve}} \frac{\tau_{xs}}{G} ds - \frac{d\phi}{dx} \cdot 2 \cdot A = 0$$

$$\oint_{\text{Closed curve}} \tau_{xs} ds = \frac{T}{J} \cdot 2 \cdot A$$

Thin-walled, One Cell

$$P(s,r) = K \cdot \left(\frac{1}{2} + \frac{r}{t} \right) + M \cdot \left(1 - \left(\frac{2r}{t} \right)^2 \right)$$

$$P(s,r) = K \cdot \left(\frac{1}{2} + \frac{r}{t} \right)$$

$$\tau_{xs} = \frac{\partial P}{\partial r} = \frac{K}{t} - \frac{8Mr}{t^2}$$

$$\tau_{xs} = P_{,r} = \frac{K}{t}$$

$$K \cdot \oint_{\Gamma_m} \frac{1}{t} ds = \frac{T}{J} \cdot 2 \cdot A_m$$

$$q_s = \tau_{xs} \cdot t = K$$

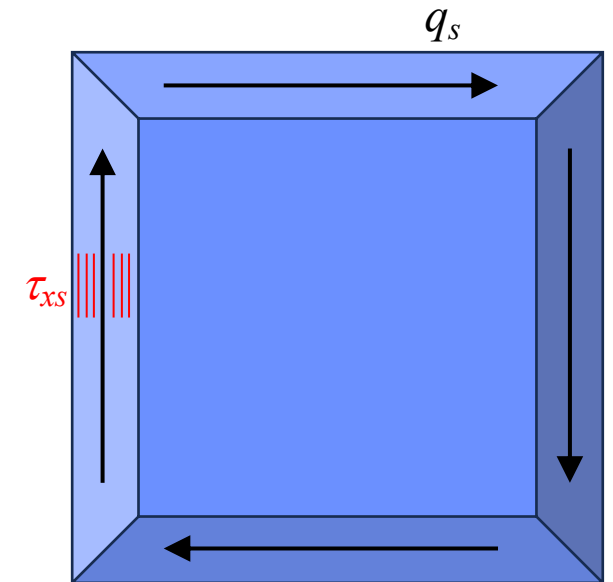
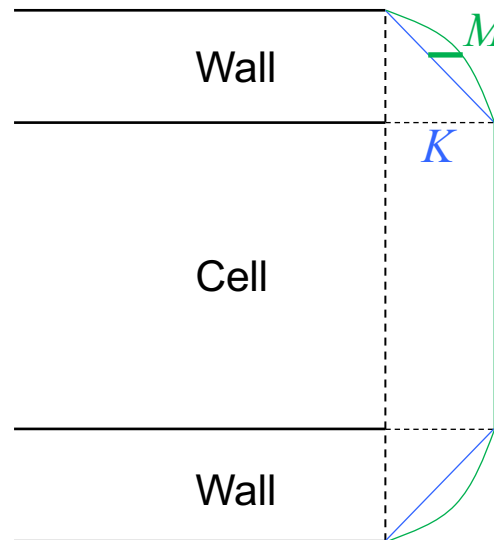
Bredt:

$$J = \frac{4 \cdot A_m^2}{\oint_{\Gamma_m} \frac{1}{t} ds}$$

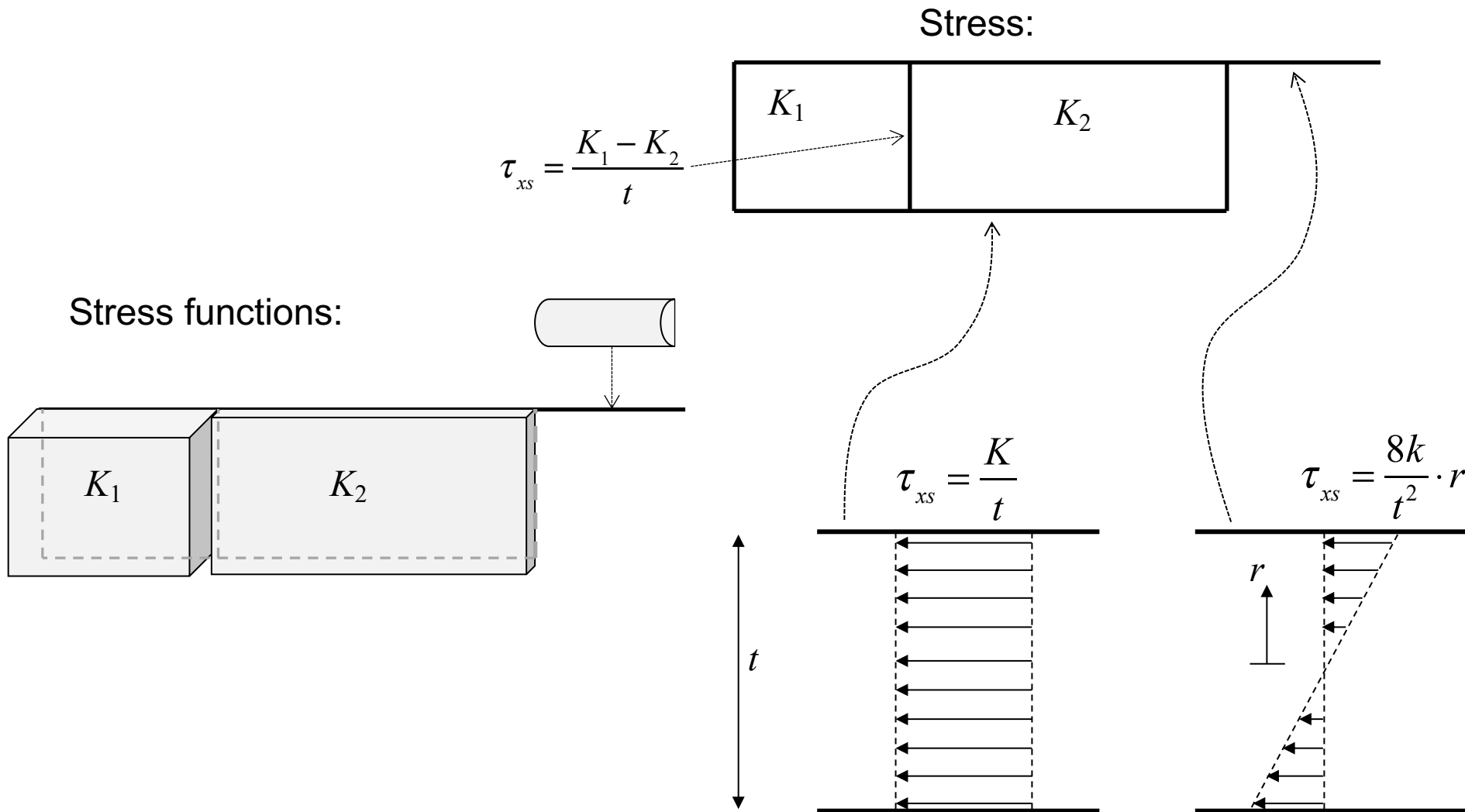
$$K \cdot \oint_{\Gamma_i} \frac{1}{t} ds - 4M \cdot \oint_{\Gamma_i} \frac{1}{t} ds = \frac{T}{J} \cdot 2 \cdot A_i$$

$$T = 2 \cdot \int_A P \cdot dA = 2 \cdot K \cdot A_m \Rightarrow K = \frac{T}{2 \cdot A_m}$$

$$M = \frac{K}{4} \cdot \left(1 - \frac{A_i}{A_m} \cdot \frac{\oint_{\Gamma_m} \frac{1}{t} ds}{\oint_{\Gamma_i} \frac{1}{t} ds} \right)$$



Visualization



More lectures:

Terje's Toolbox:

terje.civil.ubc.ca